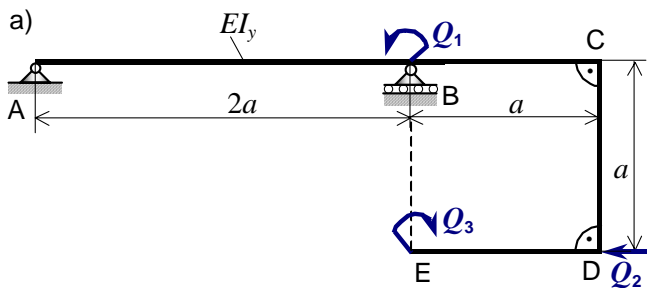


### 3. Primjer: Izračunavanje uplivnih koeficienata za ravninski okvirni nosač

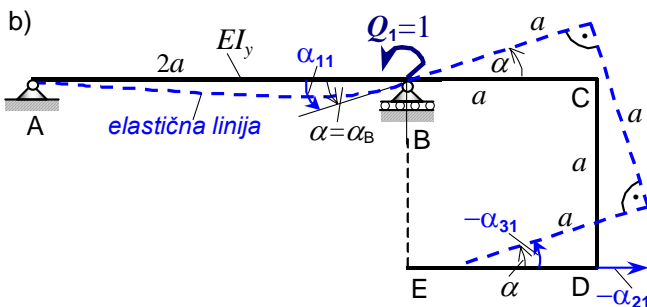


Za ravninski okvirni nosač ABCDE zadan na slici a) treba odrediti:

1. uplivne koeficijente  $\alpha_{11}, \alpha_{12}$  i  $\alpha_{13}$  primjenom metode deformacija,
2. uplivne koeficijente  $\alpha_{ij}, i, j = 1, 2, 3$ , uporabom drugog Castiglianovog poučka.

Zadano:  $a, EI_y = \text{konst.}$

Rješenje:



1. Uplivne koeficijenti  $\alpha_{11}, \alpha_{12}$  i  $\alpha_{13}$  može se odrediti pomoću tabličnih izraza u literaturi ili metodom analogne grede za vrijednost poopćene sile  $Q_1 = 1$ , slika b).

Na slici b) prikazana je elastična linija okvirnog nosača kod opterećenja nosača poopćenom silom  $Q_1 = 1$ , te deformacije na mjestima poopćenih sila  $Q_2$  i  $Q_3$ .

Kut nagiba  $\alpha$  nosača AB na mjestu oslonca B kod opterećenja jediničnim momentom na tom osloncu, slika b), pomoću tabličnog izraza jest ( $l = 2a$ ):

$$\alpha = \frac{1}{3} \cdot \frac{M \cdot l}{EI_y} = \frac{1}{3} \cdot \frac{Q_1 \cdot l}{EI_y} = \frac{1}{3} \cdot \frac{1 \cdot 2a}{EI_y} = \frac{2}{3} \cdot \frac{a}{EI_y}.$$

Uplivni su koeficijenti za opterećenje nosača poopćenom silom  $Q_1 = 1$ , slika b):

$$\alpha_{11} = \alpha = \frac{2}{3} \cdot \frac{a}{EI_y}.$$

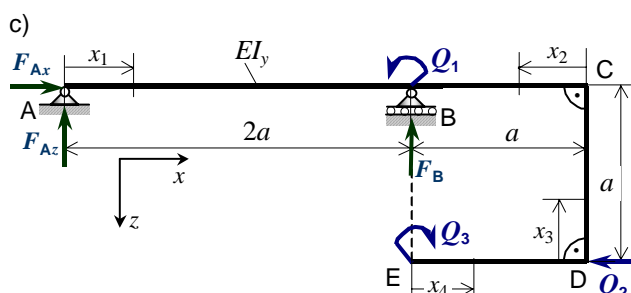
Preostali uplivni koeficijenti mogu se odrediti metodom deformacija, slika b):

$$\alpha_{12} = \alpha_{21} = -a \cdot \alpha = -\frac{2}{3} \cdot \frac{a^2}{EI_y}, \quad \alpha_{13} = \alpha_{31} = -\alpha = -\frac{2}{3} \cdot \frac{a}{EI_y}.$$

2. Određivanje uplivnih koeficienata uporabom drugog Castiglianovog poučka, kod okvirnog nosača čiji dijelovi  $l_k, k = 1, \dots, 4$  imaju  $EI_y = \text{konst.}$ , slijedi iz izraza:

$$\alpha_{ij} = \left( \frac{\partial U}{\partial Q_i} \right)_{Q_j=1} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \left( \int_0^{l_k} M_y(x_k)_{Q_j=1} \cdot \frac{\partial M_y(x_k)}{\partial Q_i} dx_k \right) \right].$$

Za određivanje momenata savijanja duž konture okvirnog nosača, potrebno je znati reakcije u osloncima nosača kod opterećenja poopćenim silama  $Q_1, Q_2$  i  $Q_3$ , slika c).



Reakcije u osloncima nosača jesu:

$$F_{Ax} = Q_2,$$

$$\sum M_B = 0 \quad -F_{Az} \cdot 2a + Q_1 - Q_2 \cdot a - Q_3 = 0 \quad / : 2a$$

$$\text{Slijedi: } F_{Az} = \frac{Q_1}{2a} - \frac{Q_2}{2} - \frac{Q_3}{2a} = F_B.$$

Momenti savijanja duž konture nosača  $M_b(x_k) = M_y(x_k)$  i potrebne derivacije jesu:

Momenti savijanja $M_y(x_k)$ :	$\frac{\partial M_y(x_k)}{\partial Q_1}$	$\frac{\partial M_y(x_k)}{\partial Q_2}$	$\frac{\partial M_y(x_k)}{\partial Q_3}$
$M_y(x_1) = F_{Az} \cdot x_1 = \frac{Q_1}{2a} \cdot x_1 - \frac{Q_2}{2} \cdot x_1 - \frac{Q_3}{2a} \cdot x_1$	$\frac{x_1}{2a}$	$-\frac{x_1}{2}$	$-\frac{x_1}{2a}$
$M_y(x_2) = -Q_2 \cdot a - Q_3$	0	-a	-1
$M_y(x_3) = -Q_2 \cdot x_3 - Q_3$	0	-x <sub>3</sub>	-1
$M_y(x_4) = -Q_3$	0	0	-1

Uplivni koeficijenti nosača uporabom drugog Castiglianovog poučka jesu:

$$\alpha_{11} = \left( \frac{\partial U}{\partial Q_1} \right)_{\substack{Q_1=1 \\ Q_2=0 \\ Q_3=0}} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \int_0^{l_k} M_y(x_k)_{\substack{Q_1=1 \\ Q_2=0 \\ Q_3=0}} \cdot \frac{\partial M_y(x_k)}{\partial Q_1} dx_k \right] = \frac{1}{EI_y} \int_0^{2a} \frac{1}{2a} \cdot x_1 \cdot \frac{x_1}{2a} dx_1 = \frac{2}{3} \cdot \frac{a}{EI_y},$$

$$\alpha_{12} = \left( \frac{\partial U}{\partial Q_1} \right)_{\substack{Q_1=0 \\ Q_2=1 \\ Q_3=0}} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \int_0^{l_k} M_y(x_k)_{\substack{Q_1=0 \\ Q_2=1 \\ Q_3=0}} \cdot \frac{\partial M_y(x_k)}{\partial Q_1} dx_k \right] = \frac{1}{EI_y} \int_0^{2a} -\frac{x_1}{2} \cdot \frac{x_1}{2a} dx_1 = -\frac{2}{3} \cdot \frac{a^2}{EI_y} = \alpha_{21},$$

$$\alpha_{13} = \left( \frac{\partial U}{\partial Q_1} \right)_{\substack{Q_1=0 \\ Q_2=0 \\ Q_3=1}} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \int_0^{l_k} M_y(x_k)_{\substack{Q_1=0 \\ Q_2=0 \\ Q_3=1}} \cdot \frac{\partial M_y(x_k)}{\partial Q_1} dx_k \right] = \frac{1}{EI_y} \int_0^{2a} -\frac{1}{2a} \cdot x_1 \cdot \frac{x_1}{2a} dx_1 = -\frac{2}{3} \cdot \frac{a}{EI_y} = \alpha_{31},$$

$$\alpha_{22} = \left( \frac{\partial U}{\partial Q_2} \right)_{\substack{Q_1=0 \\ Q_2=1 \\ Q_3=0}} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \int_0^{l_k} M_y(x_k)_{\substack{Q_1=0 \\ Q_2=1 \\ Q_3=0}} \cdot \frac{\partial M_y(x_k)}{\partial Q_2} dx_k \right] =$$

$$= \frac{1}{EI_y} \left[ \int_0^{2a} -\frac{1}{2} \cdot x_1 \cdot \frac{-x_1}{2} dx_1 + \int_0^a -a \cdot (-a) dx_2 + \int_0^a -x_3 \cdot (-x_3) dx_3 \right] = 2 \frac{a^3}{EI_y},$$

$$\alpha_{23} = \left( \frac{\partial U}{\partial Q_2} \right)_{\substack{Q_1=0 \\ Q_2=0 \\ Q_3=1}} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \int_0^{l_k} M_y(x_k)_{\substack{Q_1=0 \\ Q_2=0 \\ Q_3=1}} \cdot \frac{\partial M_y(x_k)}{\partial Q_2} dx_k \right] =$$

$$= \frac{1}{EI_y} \left[ \int_0^{2a} -\frac{1}{2a} \cdot x_1 \cdot \frac{-x_1}{2} dx_1 + \int_0^a -1 \cdot (-a) dx_2 + \int_0^a -1 \cdot (-x_3) dx_3 \right] = \frac{13}{6} \cdot \frac{a^2}{EI_y} = \alpha_{32},$$

$$\alpha_{33} = \left( \frac{\partial U}{\partial Q_3} \right)_{\substack{Q_1=0 \\ Q_2=0 \\ Q_3=1}} = \frac{1}{EI_y} \left[ \sum_{k=1}^4 \int_0^{l_k} M_y(x_k)_{\substack{Q_1=0 \\ Q_2=0 \\ Q_3=1}} \cdot \frac{\partial M_y(x_k)}{\partial Q_3} dx_k \right] =$$

$$= \frac{1}{EI_y} \left[ \int_0^{2a} -\frac{1}{2a} \cdot x_1 \cdot \frac{-x_1}{2a} dx_1 + \int_0^a -1 \cdot (-1) dx_2 + \int_0^a -1 \cdot (-1) dx_3 + \int_0^a -1 \cdot (-1) dx_4 \right] = \frac{11}{3} \cdot \frac{a}{EI_y}.$$